

		Page
Product overview	Drawn cup roller clutches	790
Features	Drawn cup roller clutches without bearing arrangement  Drawn cup roller clutches with bearing arrangement  Sealing  Lubrication  Operating temperature  Suffixes	792 792 792 792
Design and safety guidelines	Limiting load	793 793 794 795 795 798 799 799 800
Accuracy	Enveloping circle	800
Dimension tables	Drawn cup roller clutches without bearing arrangement, with and without knurling	

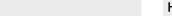


### Product overview Drawn cup roller clutches

Without bearing arrangement

With or without knurling With steel springs

HF



HF..-R





With or without knurling With plastic springs

HF..-KF

HF..-KF-R





With bearing arrangement With or without knurling With steel springs

HFL

HFL..-R





With or without knurling With plastic springs

HFL..-KF

HFL..-KF-R





#### **Features**

Drawn cup roller clutches are one-way clutches comprising thin-walled, drawn outer rings with a series of ramps on the inside diameter, plastic cages, pressure springs and needle rollers. They can transmit high torques in one direction and are particularly compact in a radial direction. The roller clutches are available with and without bearing arrangements.

Drawn cup roller clutches give very precise indexing, since the individual spring loading of the needle rollers ensures continuous contact between the shaft, needle rollers and ramps. They allow high indexing frequencies due to their low mass and the resulting low moment of inertia of the clamping elements. They also have a low overrunning frictional torque.

Drawn cup roller clutches can be used in various applications such as indexing clutches, back-stopping clutches and overrunning clutches. In these cases, the drawn cup roller clutch performs an overrunning or locking function.

## Drawn cup roller clutches without bearing arrangement

Roller clutches HF do not have a bearing arrangement and can only transmit torques.

Drawn cup roller clutches HF have steel pressure springs, while roller clutches HF..KF have plastic pressure springs.



In the case of drawn cup roller clutches without a bearing arrangement, concentricity to the shaft axis must be secured by additional rolling bearings or drawn cup roller clutches with a bearing arrangement must be used.

#### With knurling

Roller clutches with a knurled outside surface have the suffix R and are suitable for use with plastic housings.

The knurling covers all or part of the length of the drawn cup.



Drawn cup roller clutches with bearing arrangement

Roller clutches HFL have an integral plain or rolling bearing arrangement and can support torques as well as radial forces.

Drawn cup roller clutches HFL have steel pressure springs, roller clutches HFL..KF have plastic pressure springs.

With knurling

Roller clutches with a knurled outside surface have the suffix R and are suitable for use with plastic housings.

The knurling covers all or part of the length of the drawn cup.

**Sealing** 

Drawn cup roller clutches are supplied open on both sides.

Lubrication

The roller clutches are greased using a lithium soap grease to GA26. In many cases, the initial greasing is sufficient to last the operating life of the bearings.

For applications with oil lubrication, roller clutches are available without greasing. These roller clutches are coated with a preservative. Further information on lubrication: see page 799.

#### Operating temperature



Drawn cup roller clutches are suitable for operating temperatures from -10 °C to +70 °C, restricted by the grease.

**Suffixes** 

Suffixes for available designs: see table.

#### Available designs

Suffix	Description	Design		
-	Steel pressure springs	Standard		
KF	Plastic pressure springs			
R	Knurled outside surface			
RR	Drawn cup roller clutch with Corrotect <sup>®</sup> coating	Special design, available by agreement		

## Design and safety guidelines



Drawn cup roller clutches should not be used if a malfunction could lead to personal injury.

New applications, especially those involving extreme conditions, should first be verified by tests.

Correct functioning can only be guaranteed if the concentricity error between the support bearing and the shaft can be kept to a low value.

#### Limiting load



In the case of drawn cup roller clutches with plain bearings, the product of the actual speed n and the radial load  $F_r$  must not exceed the value stated for the limiting load  $(F_r \cdot n)_{max}$ .

The operating limits are determined by the limiting speeds stated in the dimension tables and the permissible radial load.

## Indexing frequency and indexing accuracy

In order not to overload the roller clutch, the inertia of the entire system must be taken into consideration. The high indexing accuracy is due to the individual spring loading of the needle rollers, which ensures continuous contact between the shaft, needle rollers and clamping surface.

The indexing accuracy is influenced by the indexing frequency, lubrication, fitting tolerances, adjacent construction, elastic deformation of the adjacent parts and the drive method, either through the shaft or the housing. Optimum accuracy is achieved if the drive is via the shaft.

#### Transmissible torque

Transmission of torque requires a rigid housing. The transmissible torque is therefore dependent on the shaft and housing material, the shaft hardness, the wall thickness of the housing and the shaft and housing tolerances.



When calculating the torque, the maximum drive torque and the moment of inertia of the masses during acceleration must be taken into consideration.



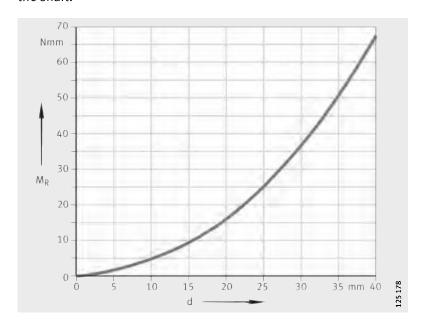
### Frictional torque and frictional energy

The frictional torque curve is shown in Figure 1.

The frictional energy during idling is dependent on whether the shaft or the outer ring is rotating, Figure 2.

Rotating outer ring

If the outer ring rotates, the frictional energy increases with speed at first but then, due to the centrifugal force of the needle rollers, it decreases gradually towards zero. At this speed, there is no longer any frictional contact between the needle rollers and the shaft. Due to the increasing centrifugal force, the needle rollers lift from the shaft.

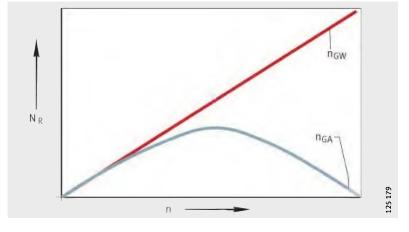


M<sub>R</sub> = frictional torque during idling d = shaft diameter

Figure 1 Frictional torque during idling, as a function of shaft diameter

n = speedN<sub>R</sub> = frictional torque during idling  $n_{GA} = limiting speed$ with rotating outer ring n<sub>GW</sub> = limiting speed with rotating shaft

Figure 2 Frictional energy during idling, as a function of speed



#### **Speeds**



The limiting speeds  $n_{\text{GW}}$  and  $n_{\text{GA}}$  in the dimension tables are valid for oil and grease lubrication.

The limiting speed  $n_{GW}$  is valid for a rotating shaft, while  $n_{GA}$  is valid for a rotating outer ring.

#### Housing design Design of housing bore

The accuracy of the locating bore essentially determines the geometrical accuracy of the drawn cup and thus the functioning of the clutch.

Housing bores must be chamfered to  $15^{\circ}$ . The bore tolerances should be produced in accordance with the table and should have a surface quality  $R_a 0.8$ .

The cylindricity tolerance of the housing bore in metal housings should be within the tolerance grade IT 5/2.

#### Tolerances for housing bore

Series	Springs	Bore					
		Housing material					
		Steel Cast iron	Light metal	Max. bore in plastic <sup>2)</sup>			
HF, HFL	Steel	N6 (N7) <sup>1)</sup>	R6 (R7) <sup>1)</sup>	_			
HFKF, HFLKF	Plastic	N7	R7	_			
HFR, HFLR	Steel	-	-	D <sub>-0,05</sub>			
HFKF-R, HFLKF-R	Plastic	_	_	D <sub>-0,05</sub>			
HFL0606-KF-R, HFL0806-KF-R	Plastic	_	_	D <sub>-0,05</sub>			

 $<sup>\</sup>overline{\mbox{The values}}$  in brackets can be used if the actual torque is no more than 50% of the permissible torque  $\mbox{M}_{\mbox{d per}}$  (see dimension tables).



<sup>2)</sup> Guide values as a function of the plastic used. Outside diameter D: see dimension tables.

#### Minimum wall thickness for metal housings

For metal housings, the maximum transmissible torque is determined as a function of the diameter ratio QA to Figure 3 (steel housing) or to Figure 4, page 797 (aluminium housing), see calculation examples.

Guide values for Q<sub>A max</sub> for steel and aluminium as housing materials are given in the table.

#### **Guide values**

Housing material	Diameter ratio Q <sub>A max</sub>		
Steel	0,8		
Aluminium	0,6		



The comparative stress  $\sigma_V$  must not exceed the yield stress of the housing material.

Steel housing calculation example

For drawn cup roller clutches HF0612, the maximum transmissible torque  $M_{d per max}$  is determined as follows:

Drawn cup roller clutch HF0612 Housing Steel Housing bore tolerance N6,

Permissible housing stress ( $R_{p0,2}$ )  $\sigma_v$ Diameter ratio Q<sub>A</sub> of housing

Permissible torque M<sub>d per</sub>

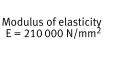
see table, page 795

450 N/mm<sup>2</sup> 0,9

see dimension table, page 801

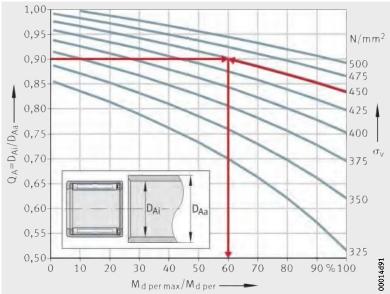
#### Calculation

$$M_{d per max} = 60\% M_{d per}$$
  
= 0,6 · 1,76 Nm  
= 1,056 Nm



 $\sigma_V$  = comparative stress  $M_{d per} = permissible torque$ (see dimension tables for values)  $M_{d per max} = maximum transmissible torque$  $Q_A$  = diameter ratio of housing  $D_{Ai}$  = housing bore D<sub>Aa</sub> = housing outside diameter

> Figure 3 Steel housing



## Aluminium housing – calculation example

For drawn cup roller clutch HF1616, the diameter ratio  $Q_A$  of the housing should be determined as follows:

Drawn cup roller clutch HF1616
Housing Aluminium

Housing bore tolerance R6,

see table, page 795 250 N/mm<sup>2</sup>

 $\begin{array}{ll} \text{Permissible housing stress } (R_{p0,2}) \ \sigma_v & 250 \ \text{N/} \\ \text{Maximum transmissible torque M}_{d \ per \ max} / \text{M}_{d \ per} & 50\% \\ & \vdots & \vdots & \vdots \\ \end{array}$ 

Permissible torque  $M_{d per}$  see dimension table,

page 801

#### Diameter ratio

$$Q_A \le 0.7 = D_{Aa} = min. 31.5$$

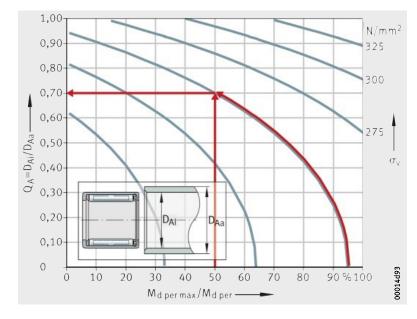
Modulus of elasticity E = 70 000 N/mm<sup>2</sup>

 $\sigma_V = \text{comparative stress} \\ M_{d \text{ per}} = \text{permissible torque} \\ \text{(see dimension tables for values)} \\ M_{d \text{ per max}} = \text{maximum transmissible torque} \\ Q_A = \text{diameter ratio of housing} \\ D_{Ai} = \text{housing bore} \\ D_{Aa} = \text{housing outside diameter} \\ \end{cases}$ 

Figure 4 Aluminium housing

## Minimum wall thickness for plastic housing

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For plastic housings, drawn cup roller clutches with a partially or fully knurled outside surface should be used (suffix R).

The guide value for the minimum wall thickness of plastic housings is:

$$s_{min} \ge D - F_w$$

s<sub>min</sub> mm Minimum wall thickness D mm Outside diameter of roller clutch F<sub>w</sub> mm Enveloping circle.

#### Shaft design

The raceway on the shaft must be hardened and ground. The surface hardness of the raceway must be 670 HV + 170 HV and the hardening depth CHD or SHD must be sufficiently large (CHD  $\geq$  0,3 mm).

The end face of the shaft must be chamfered to approx. 1 mm and 15°.

For design of the shaft, see table.

#### Shaft tolerance

Series	Springs	Shaft				
		Tolerance	Rough- ness	Round- ness	Parallelism	
			max.	max.	max.	
HF, HFL	Steel	h5 (h6) <sup>1)</sup>	R <sub>a</sub> 0,4	IT 3	IT 3	
HFKF, HFLKF	Plastic	h8	(R <sub>Z</sub> 2)			
HFR, HFLR	Steel	h5 (h6) <sup>1)</sup>				
HFKF-R, HFLKF-R	Plastic	h8				
HFL0606-KF-R, HFL0806-KF-R	Plastic	h9				

 $<sup>^{1)}</sup>$  The values in brackets can be used if the actual torque is no more than 50% of the permissible torque  $\rm M_{d~per}$  (see dimension tables).

#### **Axial location**

Drawn cup roller clutches are pressed into the housing bore and require no further axial location (assuming compliance with the recommendations according to tables, page 795).

## Sealing of the bearing position

If there is a risk of contamination, sealing rings or series G or SD should be fitted. The sealing rings are matched to the dimensions of the drawn cup roller clutches and can be combined with wider inner rings of series IR.

#### Lubrication

For general applications (mixed operation involving locking and overrunning), the Schaeffler initial greasing has proved effective.

In order to ensure optimum function, it may be necessary to use different lubricants. The suitability of the lubricant must be verified by means of tests.

For applications in which one operating condition (overrunning or locking) is heavily predominant, a special greasing should be used. In this case, please consult Schaeffler Application Engineering.

It is not possible to calculate the grease operating life or lubrication interval for drawn cup roller clutches.



If relubrication is carried out, oil should used for lubrication or a changeover to oil lubrication should generally be made.

At temperatures < –10  $^{\rm o}C$  and speeds > 0,7  $\rm n_G$  , recommendations on lubrication should be requested.

For temperatures above +70 °C, oil lubrication should be used. The oil level should be such that, when the drawn cup roller clutch is stationary and the axis is horizontal, it is immersed approx.  $^1/_3$  in the oil bath.

Suitable oils are CL and CLP to DIN 51517 or HL and HLP to DIN 51524. Viscosity classes: see table.

#### Viscosity classes

Operating temperature	Viscosity class			
+15 °C to +30 °C	ISO VG 10			
+15 °C to +90 °C	ISO VG 32			
+60 °C to +120 °C	ISO VG 100			



#### **Retention for transport**

Drawn cup roller clutches are normally packed individually in the case of small quantities.

Where larger quantities are involved, drawn cup roller clutches are placed in a specific orientation in blister packaging and delivered in this form. The blister packaging serves to retain the parts in position during transport.

## Installation using a fitting mandrel

Drawn cup roller clutches should only be pressed into the locating bore using a special fitting mandrel, see Drawn cup needle roller bearings, page 687. Attention must be paid to the clamping direction of the roller clutch. The clamping direction is indicated by an arrow on the end face of the drawn cup.



Pressing-in forces must never be directed through the rolling elements. Roller clutches should not be tilted during fitting.

#### **Guidelines for fitting**

Drawn cup roller clutches should be protected against dust, contaminants and moisture. Contaminants can impair the function and operating life of roller clutches.

#### Accuracy

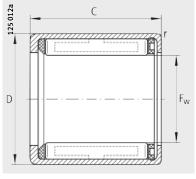
The thin-walled outer rings adopt the dimensional and geometrical accuracy of the housing bore.

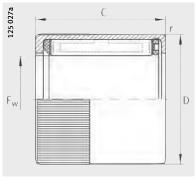
#### **Enveloping circle**

The enveloping circle is the inner inscribed circle of the needle rollers in clearance-free contact with the outer raceway.

In drawn cup roller clutches with a rolling bearing arrangement, the enveloping circle  $F_W$  of the bearings once fitted (in the solid section ring gauge) is approximately in tolerance zone F8 (for values according to table Tolerances for housing bore, page 795, and table Shaft tolerance, page 798). Deviations for tolerance zone F8: see table, page 168.

Without bearing arrangement
With or without knurling



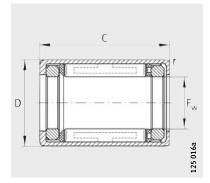


HF, HF..-KF HF..-R, HF..-KF-R With knurling

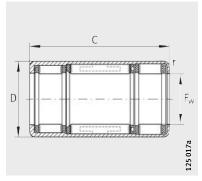
Dimension table · Dimensions in mm										
Spring design		Mass	Dimensions				Permissible torque	Limiting speeds		Drawn cup needle roller bearings
Plastic springs	Steel springs	m	F <sub>w</sub>	D	С	r	M <sub>d per</sub>	n <sub>GW</sub>	n <sub>GA</sub>	for radial bearing arrangement
Designation	Designation	≈g			-0,3	min.	Nm	min <sup>-1</sup>	min <sup>-1</sup>	Designation
HF0306-KF	_	1	3	6,5	6	0,3	0,18	45 000	8 000	HK0306-TV
HF0306-KF-R	_	1	3	6,5	6	0,3	0,06	45 000	8 000	HK0306-TV
HF0406-KF	_	1	4	8	6	0,3	0,34	34 000	8 000	HK0408
HF0406-KF-R	_	1	4	8	6	0,3	0,1	34 000	8 000	HK0408
HF0612-KF	HF0612	3	6	10	12	0,3	1,76	23 000	13 000	HK0608
HF0612-KF-R	HF0612-R	3	6	10	12	0,3	0,6	23 000	13 000	HK0608
HF0812-KF	HF0812	3,5	8	12	12	0,3	3,15	17 000	12 000	HK0808
HF0812-KF-R	HF0812-R	3,5	8	12	12	0,3	1	17 000	12 000	HK0808
HF1012-KF	HF1012	4	10	14	12	0,3	5,3	14 000	11 000	HK1010
-	HF1216	11	12	18	16	0,3	12,2	11 000	8 000	HK1212
_	HF1416	13	14	20	16	0,3	17,3	9 500	8 000	HK1412
-	HF1616	14	16	22	16	0,3	20,5	8 500	7 500	HK1612
_	HF1816	16	18	24	16	0,3	24,1	7 500	7 500	HK1812
-	HF2016	17	20	26	16	0,3	28,5	7 000	6 500	HK2010
_	HF2520	30	25	32	20	0,3	66	5 500	5 500	HK2512
_	HF3020	36	30	37	20	0,3	90	4 500	4 500	HK3012
_	HF3520	40	35	42	20	0,3	121	3 900	3 900	HK3512



With bearing arrangement With or without knurling



HFL, HFL..-KF, plain bearing arr. (HFL0308-KF, HFL0408-KF, HFL0615-KF, HFL0615)



HFL, HFL..-KF, rolling bearing arr. (F<sub>w</sub>  $\geq$  8 mm, C  $\geq$  22 mm), HFL0822-KF-R, HFL0822-R

Dimension table · Dimensions in mm							
Spring design		Mass	Dimens	ions	Permissible torque		
Plastic springs	Steel springs	m	F <sub>w</sub>	D	С	r	M <sub>d per</sub>
Designation	Designation	≈g			-0,3	min.	Nm
HFL0308-KF	_	1,4	3	6,5	8	0,3	0,18
HFL0308-KF-R	-	1,4	3	6,5	8	0,3	0,06
HFL0408-KF	-	1,6	4	8	8	0,3	0,34
HFL0408-KF-R	-	1,6	4	8	8	0,3	0,1
HFL0606-KF-R	_	1	6	10	6	0,3	0,5
HFL0615-KF	HFL0615	4	6	10	15	0,3	1,76
HFL0615-KF-R	HFL0615-R	4	6	10	15	0,3	0,6
HFL0806-KF-R	_	2	8	12	6	0,3	0,7
HFL0822-KF	HFL0822	7	8	12	22	0,3	3,15
HFL0822-KF-R	HFL0822-R	7	8	12	22	0,3	1
_	HFL1022	8	10	14	22	0,3	5,3
-	HFL1226	18	12	18	26	0,3	12,2
_	HFL1426	20	14	20	26	0,3	17,3
-	HFL1626	22	16	22	26	0,3	20,5
_	HFL1826	25	18	24	26	0,3	24,1
_	HFL2026	27	20	26	26	0,3	28,5
_	HFL2530	44	25	32	30	0,3	66
_	HFL3030	51	30	37	30	0,3	90
_	HFL3530	58	35	42	30	0,3	121

<sup>1)</sup> Attention!

Drawn cup roller clutches with plain bearing arrangement: During operation, the product of the actual speed n and the radial load  $F_r$ must not exceed the value stated for the limiting load  $(F_r \cdot n)_{max}$ . The operating limits are determined by the limiting speeds stated and the permissible radial load.

<sup>&</sup>lt;sup>2)</sup> Drawn cup roller clutches with rolling bearing arrangement.

<sup>3)</sup> No arrow on end face.